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Optimal Scaling Categorical Principal Components Analysis: Road Traffic KSI Car Accidents in England (STATS19)

Mohammad M R Sheikh

(Statistical Researcher, School of Mathematics and Computing, Kingston University London; Phone: +4407723382812, email: m.sheikh@kingston.ac.uk)

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ABSTRACT: Categorical principal component analysis (CATPCA) technique was applied in the road killed or seriously injured (KSI) car accidents in England based on STATS19 data so that the categorical variables of KSI car accidents can be transferred into few components with reduction of dimensionality. Finally selected 20 variables in KSI car accident database were divided to create four principal components by applying "optimal scaling CATPCA" procedure in SPSS. The statistically significant KSI car accident variables, particularly the most accountable categorical variables, were identified and quantified for developing models as well as leading to aims to reduce as well as to prevent the car accidents, particularly the KSI car accidents. It also leads to map out the possible safety improvement strategies as well as to inform the policymakers on how best to reduce the number and severity of car crashes.

KEYWORDS: KSI, CATPCA, optimal scaling, dimensionality, principal components, quantification

INTRODUCTION

This research is to model road traffic KSI car accidents in England based on STATS19 database by applying 'categorical principal component analysis (CATPCA)' method, so that the variables in KSI car accidents can be transferred into few components with reduction of dimensionality. CATPCA performs principal components analysis on a set of variables that can be given mixed optimal scaling levels, and the relationships among observed variables are not assumed to be linear. This technique quantifies categorical variables alongside while reducing the dimensionality of the data. The goal of CATPCA is to reduce an original set of categorical variables into a smaller set of uncorrelated components representing most of the information observed in the original variables. The technique is most useful when many categorical variables forbid effective interpretation of the relationships between objects (i.e., subjects and units), and a few components rather than many variables are interpreted by reducing the dimensionality. The optimal-scaling approach allows categorical variables to be scaled at different levels so that categorical variables are optimally quantified in the specified dimensionality, and nonlinear relationships between categorical variables can be modelled.

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The aims/ objectives of the research study are as follows:

- a) To reduce the dimensionality of categorical variables in killed or seriously injured (KSI) car accidents.
- b) To quantify the most accountable categorical variables involved in KSI car accidents.
- c) To develop models by applying categorical principal component analysis method.
- d) To inform policymakers on how best to reduce the number and severity of car crashes.

The key research questions area as follows:

- A) What are the most significant variables in road KSI car accidents?
- B) How can these KSI car accidents be reduced?

The structure of the study is detailed as **Section 2** is research methods including data source, CATPCA method, defining scale and weight of variables, discretisation, missing vale option, output/ loading plots etc. **Section 3** is a brief of KSI car accident database construction and data manipulation extracted from STATS19 database. **Section 4** is CATPCA application in KSI car accidents, including design, variable selection, iteration, quantification, variance accounted for (VAF), rotated variance accounted for (RVAF), correlation matrix of original variables as well as transformed variables, and component loadings as well as rotated component loadings. **Section 5** is study findings, discussions, and conclusion.

2. RESEARCH METHODS

2.0. Data Source

The study is to use the secondary data from DfT-STATS19 database developed by UK Police and Department of Transport, UK. The DfT has undertaken work to link data from STATS19. Data for KSI car accidents in England are to be extracted from the DfT-STATS19 database. This secondary data covers the period from 1979 through 2015.

2.1. CATPCA Method

The CATPCA simultaneously not only quantifies categorical variables, but also decreases the dimensionality of the data. It is to bring down an original set of variables into a smaller set of uncorrelated components, representing most of the information found in the original variables. The technique is most useful in STATS19 data as many variables exclude effective interpretation of the relationships between subjects and units. The optimal-scaling approach allows variables to be scaled at different levels so that categorical variables are optimally quantified in the specified dimensionality as well as nonlinear relationships between variables can be modelled.

In CATPCA data considerations, string variable values are always converted into positive integers by ascending alphanumeric order, where user-defined missing values or systemmissing values or any values less than 1 are considered missing. The data contain at least three valid cases mandatorily and it must be positive integer. The discretization option is to automatically categorise a fractional-valued variable by grouping its values into categories with a close to "normal" distribution and it is to automatically convert values of string variables into positive integers.

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2.2. Defining Scale and Weight of Variables in CATPCA

Optimal scaling level is set for analysis variables and supplementary variables, as well as the weight for analysis variables can be set specifying a positive integer. The scaling level to be used to quantify each variable can also be selected so that a) the order of the categories of the observed ordinal variable is preserved in the optimally scaled variable; b) the order of the categories and the equal distances between category numbers of the observed discrete variable are preserved in the optimally scaled variable.

2.3. Discretisation in CATPCA

The variables are to be discretised by applying 'grouping method', where a specified number of categories is recoded for categorical variables as well as discrete variables are recoded into categories defined by equally sized intervals.

2.4. Missing Values in CATPCA

Missing values with the quantification of an extra category can be replaced so that objects with a missing value on the variable are considered to belong to the same (extra) category.

2.5. Options in CATPCA

The Options provide the controls to select the initial configuration, specify iteration and convergence criteria, as well as to select a normalisation method, to choose the method for labelling plots, and to specify supplementary objects. The case number of the object, or the first and last case numbers of a range of objects to make supplementary, is specified if it is needed. If an object is specified as supplementary, then case weights are ignored for that object. One of ¹five options (i.e., Variable Principal, Object Principal, Symmetrical, Independent and Custom) for normalising the object scores and the variables, is specified. It is noted that only one normalisation method can be used in each analysis.

The maximum number of iterations can be specified so that the procedure can go through in its computations. A convergence criterion value can also be selected. The algorithm stops iterating when the difference in total fit between the last two iterations is less than the convergence value or if the maximum number of iterations is reached. Variables and value labels or variable names

¹ Normalising Methods:

a) **Variable Principal** option is applied to optimise the association between variables so that the coordinates of the variables in the object space are the component loadings (correlations with principal components, such as dimensions and object scores).

b) **Object Principal** option is applied to optimise the distances between objects.

c) Symmetrical option is used for the relationship between objects and variables.

d) **Independent** option is used to examine distances between objects and correlations between variables separately.

e) **Custom** option specifies any real value in the closed interval [-1, 1] where value of '1' is for the Object Principal option; '0' is for the Symmetrical option; '-1' is for the Variable Principal option. Any value greater than '-1' or less than '1' is specified so that the eigenvalue over both objects and variables are spreaded.

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and values can be specified to be used in the plots. All dimensions in the solution are displayed in a scatterplot matrix. One of ²five options for rotation method (i.e., Varimax, Quartimax, Equamax, Oblimin and Promax) to obtain rotated results, can be selected.

2.6. Output and Loading Plots in CATPCA

- 1) Displays the component loadings for all variables that were not given multiple nominal scaling levels. The component loadings by size can be sorted. The component loadings can be displayed in Scatter Matrix.
- 2) Shows for each iteration, the variance accounted for, loss, and increase in variance accounted for (VAF).
- 3) Shows the correlation matrix of the original variables and the eigenvalues of that matrix.
- 4) Shows the correlation matrix of the transformed (optimally scaled) variables and the eigenvalues of that matrix.
- 5) Displays the amount of variance accounted for (VAF) by centroid coordinates, vector coordinates, and total (centroid and vector coordinates combined) per variable and per dimension. The VAF can be shown in Bar Charts.
- 6) Gives the category quantifications and coordinates for each dimension of the variables that are selected.

3. Road KSI Car Accident Data Manipulation and Database Construction

The reported/ recorded data of road traffic KSI car accidents extracted from the datasets of DfT-STATS19 under Department for Transport for the period of 1979-2015, had been used for database construction and then, the data in the databases were manipulated individually using 'data function' and 'transform function' of SPSS 26.0.1 version and onwards following research methodology as briefed in the previous section (i.e., Section 2).

Two accident databases based on DfT-STATS19 database, were constructed containing the existing variables and the new variables computed from existing variable(s) following the database design such as determining the purpose of the database, findings, and organising the information required, dividing the information items into tables, turning information items into

² Rotated Methods:

f) **Varimax** orthogonal rotation method is to minimise the number of variables to have high loadings on each component.

g) **Quartimax** rotation method is to minimise the number of components that are needed to explain each variable.

h) **Equamax** rotation method is a combination of the Varimax method, and the Quartimax method so that the number of variables loading highly on a component and the number of components needing to explain a variable, are minimised.

i) **Oblimin** is a method for oblique (non-orthogonal) rotation. The value of Delta must be less than or equal to 0.8.

j) **Promax** is an oblique (non-orthogonal) rotation, to allow the components to be correlated. The amount of correlation (obliqueness) that is allowed is controlled by the kappa parameter. The value of **Kappa** must be greater than or equal to 1 and less 10,000.

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columns, specifying the primary keys, applying the normalisation rules, refining the design and setting up the table relationship.

Total 49 variables, containing 10 discrete variables as well as 13 dichotomous, 14 nominal and 12 ordinals, were included in road KSI car accident database shown in Table 3.

| Table 3. | Valid/ Missing | KSI cases | in Road | Car Acciden | t Data | based in | n Accident | Index | in |
|----------|----------------|-----------|---------|-------------|--------|----------|------------|-------|----|
| | | | En | oland | | | | | |

| | Valid and Missing KSI Cases in | Road Traffic | Car Accider | vt Database bas | sed on Accidem | Index in England | | |
|--------------|---|--------------|-------------|-----------------|---------------------|------------------|------------|--------------|
| | Variable/ Factor | Type | Valid Case | Valid Case % | Missing Case | Missing Case % | Other Case | Other Case % |
| 1 Accident | Year | Continuous | 1089560 | 100.00 | 0 | £0.00 | 0 | 0.00 |
| 2 First Roa | ad Number | Continuous | 815907 | 74.90 | 273653 | £25.10 | 0 | 0.00 |
| 3 Latitude | | Continuous | 332388 | 30.51 | 757172 | £69.49 | 0 | 0.00 |
| 4 Longitud | erre come contra com | Continuous | 332388 | 30.51 | 757172 | 669.49 | 0 | 0.00 |
| 5 Number | of Casualty per KSI Accident | Continuous | 1089560 | 0.00 | 0 | £0.00 | 0 | 0.00 |
| 6 Number | of Vehicle per KSI Accident | Continuous | 1089560 | 0.00 | 0 | £0.00 | 0 | 0.00 |
| 7 OSGR E | asting | Continuous | 1086224 | 99.69 | 3336 | £0.31 | 0 | 0.00 |
| 8 OSGR N | lorthing | Continuous | 1087795 | 99.84 | 1764 | £0.16 | 0 | 0.00 |
| 9 Second I | Road Number | Continuous | 1069885 | 98.19 | 19675 | £1.81 | 0 | 0.00 |
| 10 Speed Li | mt | Continuous | 1089560 | 100.00 | 0 | £0.00 | 74 | 0.00 |
| 11 Built-non | -Built-up Speed Area | Dichotomous | 1089557 | 100.00 | 3 | £0.00 | 0 | 0.00 |
| 12 Carriage | way Hazards-non-Hazards | Dichotomous | 1082347 | 99.30 | 7213 | £0.70 | 0 | 0.00 |
| 13 First Cla | ssified-non-Classified Road Class | Dichotomous | 1089560 | 100.00 | 0 | £0.00 | 0 | 0.00 |
| 14 First Cla | ssified Trunk-non-Trunk Road Class | Dichotomous | 797819 | 73.20 | 291741 | £26.80 | 0 | 0.00 |
| 15 First Nur | nbered-non-Numbered Road | Dichotomous | 1089505 | 100.00 | 55 | £0.00 | 0 | 0.00 |
| 16 Junction | Control-non-Control | Dichotomous | 607766 | 55 80 | 481794 | £44 20 | 0 | 0.00 |
| 17 Junction | -non-Junction Details | Dichotomous | 1089471 | 100.00 | 89 | £0 00 | 0 | 0.00 |
| 18 Pedestra | an Crossing at Human Control | Dichotomous | 3450 | 0.30 | 100 | £0.00 | 0 | 0.00 |
| 19 Pedestra | an Crossing at Human Control-non-Control | Dichotomous | 1069982 | 98.20 | 100 | £0.00 | 0 | 0.00 |
| 20 Pedestri | an Crossing at Physical-non-Physical Facilities | Dichotomous | 1069890 | 98.20 | 19670 | £1.90 | 0 | 0.00 |
| 21 Police O | fficer's Attandance-non-Attendance at Accident Sc | Dichotomous | 321525 | 29.50 | 769035 | £70.50 | 0 | 0.00 |
| 22 Road En | wronment Urban-non-Urban | Dichotomous | 479962 | 44.00 | 609698 | £56.00 | 0 | 0.00 |
| 23 Special (| Conditions non-Conditions at Site | Dichotomous | 1067904 | 98.00 | 21656 | \$2.00 | 0 | 0.00 |
| 24 Carriane | way Hazards (5-I evel) | Nominal | 18983 | 1.70 | 7213 | E0 70 | 1063364 | 97.60 |
| 25 First Cla | ssified Road Class (5-) even | Nomial | 797819 | 73.20 | 100 | 50.00 | 291741 | 26.80 |
| 26 England | Region (9-1 evel) | Nomial | 1089560 | 100.00 | 100 | \$0.00 | 0 | 0.00 |
| 27 Junction | Control (4.1 evel) | Nomial | 596831 | 54.80 | 481794 | £44.20 | 10936 | 1.00 |
| 28 Junction | Detais (R.Level) | Nomial | 597571 | 54.90 | 89 | \$0.00 | 491900 | 45.10 |
| 29 Linhts C | antitions (5.1 evel) | Nomial | 1089413 | 100.00 | 147 | F0.00 | 0 | 0.00 |
| 30 Pedectro | an Crossion at Physical Earlities (5.) evel) | Nomial | 134018 | 12.30 | 19870 | £1.90 | 935974 | 85.90 |
| 31 Police O | ficer's Mandance at Accident Scene (3.1 evel) | Nominal | 321525 | 29.50 | 789035 | £70.50 | 0 | 0.00 |
| 32 Read En | wronment (3.) evel) | Nomial | 479962 | 44.00 | 809898 | £58.00 | 0 | 0.00 |
| 33 Road St | dace Conditions (7.1 mail) | Mornial | 1089290 | 00.00 | 1270 | 50.10 | 0 | 0.00 |
| 34 Road Tu | na (5.1 aval) | Nomial | 1070965 | 98.30 | 18505 | £1.70 | 0 | 0.00 |
| 35 Second I | Road Class (5.1 avail) | Nomial | 578347 | 53.10 | 511213 | E46 90 | 0 | 0.00 |
| 36 Special (| Conditions at Site (7.1 evel) | Nomial | 19601 | 1.90 | 21056 | £2.00 | 1048213 | 96.20 |
| 37 Weather | Conditions (8.1 evel) | Nomial | 1089460 | 100.00 | 100 | 50.00 | 0 | 0.00 |
| 29 Accident | Day (7.1 min) | Ordenal | 1000560 | 100.00 | 100 | 60.00 | 0 | 0.00 |
| 29 Accident | Month (12.1 mml) | Ordinal | 1009560 | 100.00 | 100 | 00 00 | 0 | 0.00 |
| 40 Accident | Time (12.1 and) | Ordinal | 1009472 | 100.00 | 89 | 50.00 | 0 | 0.00 |
| 41 Car per l | KSI Accident (2.1 minl) | Owlead | 1000560 | 500.00 | 100 | 50.00 | 0 | 0.00 |
| 47 Cacualty | ner KSI Car Areidart ("Li mall | Ordeal | 1080500 | 100.00 | 100 | 50.00 | 0 | 0.00 |
| 43 First Nur | whered Road Cint (S.) evel | Ordinal | 815007 | 74.90 | 100 | 50.00 | 273508 | 25.10 |
| 44 First Abu | nhered Road Zone (4.1 puel) | Ordinal | 703467 | 72.80 | 22406 | 52.10 | 273568 | -25 10 |
| d5 Loth de | Band (61 each) | Ordinal | 332284 | 30.60 | 757470 | CC0 ER | 210000 | 0.00 |
| 46 Longitud | e Band (5.1 evel) | Ordenai | 332300 | 30.50 | 767479 | 600.00 | 0 | 0.00 |
| 47 OSCP C | action Band (5.) evel | Ordinal | 1096224 | 90.70 | 2228 | 20 20 | 0 | 0.00 |
| 49 0900 N | lothing Dand (7 Laugh | Ordenal | 1000224 | 00.00 | 4704 | £0.30 60.30 | 0 | 0.00 |
| 40 USGR N | and (7-cevel) | Ordeni | 1007/90 | 100.00 | 1/04 | 20.20 | 0 | 0.00 |

4. CATPCA in KSI Car Accidents

By following El-Basyouny and Sayed (2009), Harrel (2015), Kleinbaum and Klein (2010), Saukani and Ismail (2019), and Hung and Tai-Jin. (2018), categorical principal component analysis (CATPCA) method was applied in KSI car accidents.

4.0. CATPCA Design

The CATPCA based on "optimal scaling level for one set of variables that some factor(s) are not niminal" was run on a 20-factor/ factor dataset that measured desired 'road traffic KSI car

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accident' characteristics on 1089560 cases/ observations. The suitability of CATPCA was assessed prior to analysis. Inspection of the correlation matrix showed that all variables had at least one correlation coefficient greater than 0.3. Grouping method and normal distribution were used for discretisation. The methods such as 'factor principal' and 'Varimax for rotation with Kaiser nomalisation' were applied. Each factor was defined/ scaled as '1' for its weight that was analysed through optimal scaling level. Preliminary assumption checking revealed: variables were measured in ordinal/ nominal/ dichotomous formats; there were linear relationships between all variables, as assessed by scatterplots; the data had sampling adequacy (large sample size, n = 1089560); the dataset were suitable for data reduction; there should be no significant outlier(s), as assessed by boxplot.

4.1. Variables in CATPCA of Car Accidents

1089560 cases of 20 variables were used in analysis, where the common cases that were valid were 579496.

- a) Only one discrete variable such as 'accident year' was used.
- b) Seven dichotomous variables such as 'built-non-built up speed area', 'carriageway hazards-non hazards', 'junction-non-junction details', 'junction control-non-control', 'pedestrian crossing at human control-non-control', 'pedestrian crossing at physical-non-physical facilities', and 'special conditions-non-conditions', were used.
- c) Four nominal variables such as 'England region', 'lighting conditions', 'road type', and 'weather conditions', were used.
- d) Eight ordinal variables such as 'OSGR easting band', 'OSGR northing band', 'speed limit zone', 'casualty per accident', 'car per accident', 'accident time', 'accident day', and 'accident month', are used.

4.2. Iterations in CATPCA of Car Accidents

The process stopped at the 34th iteration because the convergence test value was reached. The iteration history has been displayed in Table 4.2. The 0th iteration displays the solutions of the statistics with all variables. It displays the eigenvalues for each iteration of the analysis. These are used to determine the percentage of variance accounted for (a type of effect size) and therefore, larger eigenvalues are preferred over smaller ones to get a better solution (higher eigenvalue).

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| Iteration Number | Variance Ac | counted For | 111111111111 | | Loss |
|----------------------|----------------|-------------------|--------------|--|--|
| | Total | Increase | Total | Centrold Coordinates | Restriction of Centroid to Vector Coordinates |
| 0 | 6.33255 | 0.00151 | 73.667 | 72.134 | 1.5329 |
| 1 | 7.09878 | 0.76623 | 72.901 | 72.134 | 0.7667 |
| 2 | 7.37783 | 0.27905 | 72.622 | 71.793 | 0.8291 |
| 3 | 7.47787 | 0.10004 | 72.522 | 71.718 | 0.8044 |
| 4 | 7.53631 | 0.05844 | 72.464 | 71.683 | 0.7810 |
| 5 | 7.57372 | 0.03741 | 72.426 | 71.662 | 0.7635 |
| 6 | 7.60111 | 0.02739 | 72.399 | 71.646 | 0.7524 |
| 7 | 7.62449 | 0.02338 | 72.376 | 71.629 | 0.7461 |
| 8 | 7.64729 | 0.02280 | 72.353 | 71.608 | 0.7446 |
| 9 | 7.67190 | 0.02460 | 72.328 | 71.581 | 0.7476 |
| 10 | 7.70020 | 0.02830 | 72.300 | 71.545 | 0.7546 |
| 11 | 7.73325 | 0.03306 | 72.267 | 71.502 | 0.7650 |
| 12 | 7.77106 | 0.03781 | 72.229 | 71.452 | 0.7774 |
| 13 | 7.81209 | 0.04103 | 72.188 | 71.398 | 0.7900 |
| 14 | 7.85318 | 0.04109 | 72.147 | 71.345 | 0.8013 |
| 15 | 7.89036 | 0.03718 | 72.110 | 71,299 | 0.8108 |
| 16 | 7.92060 | 0.03024 | 72.079 | 71.261 | 0.8185 |
| 17 | 7.94300 | 0.02240 | 72.057 | 71.232 | 0.8245 |
| 18 | 7.95850 | 0.01550 | 72.042 | 71.212 | 0.8293 |
| 19 | 7.96873 | 0.01023 | 72.031 | 71.198 | 0.8329 |
| 20 | 7.97518 | 0.00646 | 72.025 | 71.189 | 0.8358 |
| 21 | 7.97916 | 0.00398 | 72.021 | 71.183 | 0.8381 |
| 22 | 7.98161 | 0.00245 | 72.018 | 71,179 | 0.8399 |
| 23 | 7.98313 | 0.00152 | 72.017 | 71.176 | 0.8413 |
| 24 | 7.98408 | 0.00095 | 72.016 | 71.174 | 0.8424 |
| 25 | 7.98467 | 0.00060 | 72.015 | 71.172 | 0.8432 |
| 26 | 7.98506 | 0.00038 | 72.015 | 71.171 | 0.8439 |
| 27 | 7.98530 | 0.00024 | 72.015 | 71.170 | 0.8444 |
| 28 | 7.98546 | 0.00016 | 72.015 | 71.170 | 0.8449 |
| 29 | 7.98556 | 0.00010 | 72.014 | 71.169 | 0.8452 |
| 30 | 7.985624 | 0.000067 | 72.014 | 71.169 | 0.8455 |
| 31 | 7.98567 | 0.000044 | 72.014 | 71.169 | 0.8457 |
| 32 | 7.98570 | 0.000028 | 72.014 | 71.168 | 0.8458 |
| 33 | 7.98571 | 0.000014 | 72.014 | 71.168 | 0.8455 |
| 34 | 7.98572 | 0.000008 | 72.014 | 71.168 | 0.8459 |
| Iteration 0 displays | the statistics | of the solution w | th all vari | ables, except variables v as numerical. | vith optimal scaling level Multiple Nominal, treated |

4.3. Quantification of Variables in CATPCA of Car Accidents

The quantification for dichotomous variables followed by nominal and ordinal variables, is detailed and displayed in Table 4.3 that display the frequency, the quantification value assigned, the centroid coordinates, and the vector coordinates of each response category for each item.

Table 4.3. Quantification in CATPCA of KSI Car Accidents in England

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| Variable | Variable | Category | Frequency | Quantification | Ce | ntroid C Dime | oordina naion | nteo | Ve | Dime | ordinab naion | *5 |
|----------|--|--|------------------|----------------|--------|------------------|------------------|--------|--------|-----------------|------------------|--------|
| .9104 | | and Pulling Record Anno | accasa | | 1 444 | 2 | 3 | 4 | 1 1000 | 2 | 3 | 4 |
| | Buit-non-Sull up Speed Area | Bull up Speed Area | 735954 | 0.686 | 0.597 | 0.052 | 0.109 | 0.098 | 0.595 | 0.026 | 0.127 | 0.068 |
| | Carriageway Hazards | No Hazards | 1063364 | 0.025 | 0.002 | 0.008 | 0.001 | 0.016 | <0.001 | 0.001 | 8.003 | -0.001 |
| | non-Hazarda | Hazards- Missing | 18963 | 7.574 | -0.136 | -0.359 | -0.924 | 0.040 | -0.137 | 10.300 | -0.924 | 0.035 |
| | Junction Control-non- | Not at Junction or Within 20 Metres | 10930 | -3.530 | -0.622 | 0.436 | -1.993 | -0.661 | 0.703 | 0.032 | 1.971 | -0.200 |
| 5 | Control | As Junction or Within 20 Mades Missing | 481794 | 3.294 | 0.201 | 0.009 | 0.704 | 0.054 | 0.252 | -0.011 | 0.00 | 0.075 |
| 8 | Junction non Junction | Not al Junction or within 20 Metres | 491900 | -1 126 | 0.331 | -0.009 | -0.900 | -0.031 | -0.331 | -0.010 | -8.850 | -0.045 |
| chat | Details | Missing | 50/5/1 | 0.003 | 0.200 | 4010 | 0.704 | 0.00+ | 0.760 | 0.000 | 0.106 | 11.0.5 |
| | Pedestriat Crossing at Haman Costrol.nos. | Not at Crossing or within 50 Metres | 1005432 | 1011 | 0.011 | 800 D. | 0.017 | -0.089 | 0.011 | 0.008 | 0.0017 | 0.02 |
| | Control | Missing | 19678 | | | | | | | | | |
| | at Physical-non- | At Physical Crossing Facilities or within 50 Methes At Physical Crossing Facilities or within 50 Methes | 134016 | 2,666 | 1.077 | 0.279 | 0.191 | -0.073 | 1.081 | 0.287 | 0.208 | -0.10 |
| | Physical Facilities | Missing No. Contribute | 1045213 | 0.088 | 0.005 | 0.009 | 0.015 | .0.007 | 0.014 | 8.010 | .8.017 | .0.00 |
| | Special Conditions non-Conditions at Site | Special Conditions | 19091 | 1.891 | -0.287 | -0.053 | -0.063 | -0.135 | 0.028 | -0.019 | -0.032 | -0.58 |
| | | North-East Region | 21656 | .1.452 | 0.142 | -1,400 | .0.009 | -0.154 | -0.152 | .1.355 | 0.053 | .0.15 |
| | | North-West Region Vortestary & the Hamber Breaks | 101051 | -0.000 | 0.203 | -0.078 | -0.032 | -0.010 | -0.006 | -0.056 | -0.002 | -0.000 |
| | | East Midlands Region | 99862 | -1,369 | 0.186 | -1277 | -0.027 | -0.097 | 0.142 | -1.271 | 0.050 | -8.17 |
| | England Region | West Midlands Region Eastern Rection | 117766 | 0.829 | 0.044 | -0.813 | -0.052 | 0.072 | 0.087 | -0.775 0.085 | -8.630 | -8.20 |
| | | Landon Regran | 170391 | 1.664 | 0.563 | 1.478 | 0.120 | 0.460 | 0.174 | 1.556 | 0.061 | 0.21 |
| | | South-East Region | 178554 | 0.548 | -0.310 | 0.585 | -0.005 | -0.079 | 0.057 | 0.513 | 0.020 | 0.00 |
| | | Darkness with Lights Lit | 278734 | -0.819 | 0.555 | 0.007 | 0.001 | 0.137 | 0.432 | -0.005 | 0.240 | 0.64 |
| | Lighting Conditions | Darkness without Lighting | 100015 | 2:997 | 1.490 | 0.030 | -1.043 | -0.100 | -1.579 | 0.022 | 0.880 | -0.17 |
| - | | Definess with Lighting Unknown. Deviate | 8761 695378 | 0.067 | 0.085 | -0.098 | 0.299 | 0.202 | 0.030 | +0:001 | 0.021 | -8.00 |
| 10 | | Missing | 147 | | | | | | | | | |
| 2 | | Roundatiout Dual Carriageway | 140963 | -0.246 | 0.180 | 0.046 | 0.713 | -0.184 | -0.006 | -0.014 | 0.009 | -0.210 |
| | Road Type | One Way Street Slip Road | 4333 | 1311 | 0.542 | 0.115 | 0119 | 1 105 | 0.030 | 0.075 | 0.057 | 1.95 |
| | | Single Carriageway | 880090 | -0.068 | 0.029 | -0.026 | -0.014 | -0.009 | -0.002 | -0.004 | 0.003 | -0.05 |
| | | Missing Baining without Hinth Wants | 18595 | 0.143 | 0.035 | 0.021 | 0.015 | 0.112 | 0.005 | 0.006 | 0.010 | 0.54 |
| | | Browing without High Winds | 5808 | 0.414 | -0.237 | -0.237 | -0.285 | 0.317 | 0.013 | 0.017 | -0.028 | 0.33 |
| | | Fine with High Winds Baining with High Winds | 15156 | -0.064 | 0.160 | -0.177 | -0.118 | -0.051 | 0.002 | -0.002 | 0.004 | -0.04 |
| | Weather Conditions | Showing with high Winds | 1629 | 0.209 | -0.560 | -0.378 | 0.380 | 0.135 | 0.007 | 0.009 | 0.014 | 0.16 |
| | | Other Unknown WC | 45003 | 4,735 | 0.034 | 0.200 | -0.330 | 3809 | -0.153 | 0.003 | -0.005 | 3.80 |
| | | Fine without High Winds Mission | 853096 | -0.252 | 0.021 | -0.004 | 0.006 | -0.203 | 0.008 | -0.011 | 0.017 | -0.203 |
| | | CSE 0-300 km | 44900 | -0.812 | 0.185 | 0.425 | -0.163 | 1.367 | 0.031 | 0.561 | -8.002 | 0.05 |
| | | OSE 300-400 km OSE 500-600 km | 246730 345640 | -0.812 | 0.002 | 0.927 | 0.052 | 0.103 | 0.031 | 0.561 | -8 002 | 0.051 |
| | GSGH Easting Band | C65E 800-700 km | 30062 | -0.198 | 0.283 | 0 153 | -0.011 | 0.010 | 0.008 | 0.137 | =0.001 | 0.012 |
| | | Missing | 3336 | 1,670 | 11.040 | 0.000 | didu's | 9.000 | 0.049 | 4.00.5 | 0.004 | 0.00 |
| | | OSN 0.100 km OSN 200.300 km | 53020 | -0.737 | 0.118 | 0.018 | -0.051 | 0.282 | -0.041 | -0.607 | -0.028 | 0.096 |
| | | CSN 300-400 km | 203295 | -0.737 | 0.000 | -0.679 | -0.019 | 0.002 | 0.041 | 0.607 | -0.028 | 0.096 |
| | OSGR Nothing Band | CEN 400-500 km | 1582/4 | -0.737 | 0.120 | -0.738 | -0.016 | 0.156 | 0.041 | -0.607 | -0.028 | 0.098 |
| | | CGN 000+ km | 13645 | -0.737 | 0.055 | 0.056 | -0.158 | 3 598 | -0-041 | -0.607 | -0.020 | 0.096 |
| | | Messing | 1754 | 1,401 | | | 0.001 | | a arr | 1.161 | 0.021 | |
| | | 20 mph (32 km/h) Zone 40 mph (64 km/h) Zone | 3029 | -1 193 | 0.114 | 840.0. | 0.185 | -0.367 | -1:009 | -0.062 | -0.182 -0.182 | .0.130 |
| | Council Limit Trees | 50 mph (90 km/h) Zone | 19878 | -1.193 | -1.079 | 0.212 | -0.087 | -0.289 | -1.009 | -0.062 | -0.182 | -0.130 |
| | Speed Child Zone | 70 mph (112 km/h) Zone | 78668 | -1.193 | 1.218 | -0.050 | -0.406 | -0.137 | -1.009 | -0.062 | -0.162 | -0.13 |
| | | 30 mph (48 km/li) Zonk Missimi | 636228 | 0.835 | 0.767 | 8.045 | 0.188 | 0.112 | 0.706 | 0.043 | 0.127 | 0.09 |
| | Casualty per KSI Car | Single Crowsby | 729623 | -0.682 | 0.308 | 0.005 | 0.123 | 0.011 | 0.374 | 0.005 | 0.100 | -0.00 |
| | Accident | Double Casualties Multiple Casualties | 204861 154876 | 1.045 | 1.022 | 0.010 | 0.153 | 0.025 | -1.012 | 0.009 | 0.154 | 0.00 |
| | Car per 651 Accedent | Single Car Double Car | 415843 | -1.287 | 0.523 | 0.054 | -0.815 | -0.003 | 0.546 | -0.065 | 0.799 | -0.010 |
| | our por rear activitient | Multiple Cars | 116199 | 0.949 | 0.730 | 0.025 | 0.367 | 0.013 | -0.402 | 0.048 | 0.589 | 0.01 |
| | | AT(02:01-02:00) AT(02:01-04:00) | 46265 | -3.521 | 0.150 | 0 129 | -1.331 | 0.040 | D 163 | 0.136 | -1.350 | -8.009 |
| | | A104-01-0000 | 14200 | -2.818 | -0.014 | 0.142 | -1.101 | -0.071 | 0.131 | 0.109 | -1.088 | -0.00 |
| | | AT(05:01:00:00) AT(05:01:10:00) | 98236 | 9.722 | 0.219 | 0.053 | 0.158 | 0.001 | 0.010 | 0.009 | 0.006 | <0.00 |
| | Accodent Time | AT(10:01-12:00) AT(12:01-14:00) | 86294 | 0.222 | 0.058 | 0.018 | 0.148 | -0.028 | 0.010 | -0.009 | 0.086 | <0.00 |
| | Physical street | AT(14:01-16:00) | 132191 | 0.222 | 0.007 | -0.628 | 0.070 | -0.014 | -0.010 | -0.009 | 0.086 | <8.00 |
| | | A7(18:01-20:00) A7(20:01-22:00) | 136823 | 0.222 | 0.028 | 0.013 | 0.088 | 0.007 | -0.010 | -0.009 | 0.086 | -0.00 |
| | | AT(22:01:00:00) | 102938 | 0.222 | -0.039 | 0.015 | -0.103 | 0.127 | 0.010 | -0.009 | 0.088 | -0.00 |
| | | Missing | 101057 | 0.357 | 0.030 | 0.067 | 0.136 | 0.019 | -0.036 | -0.014 | 0 130 | ×0.00 |
| | | Sunday Monday | 143338 | -2.605 | 0.126 | 0.028 | 0.392 | 0.028 | 0.126 | 0.028 | 0.390 | 0.019 |
| | and a second second second | Tuesday | 143945 | 0.243 | 0.033 | 0.009 | 0.085 | 0.009 | 0.011 | -0.003 | 0.030 | -0.000 |
| | Accident Day | Wednesday | 147130 | 0.243 | 0.011 | 0.008 | 0.091 | 0.007 | 0.011 | -0.003 | 0.036 | -0.000 |
| | | Baturday | 171857 | 0.243 | -0.012 | -0.011 | -0.111 | 0.013 | 0.011 | -0.003 | 0.038 | -0.000 |
| | | January | 87000 | 0.243 | 0.012 | 0.012 | 0.005 | 0.047 | 0.011 | 0.004 | 0.000 | -0.000 |
| | | February March | 77658 | 0.221 | 0.020 | 0.005 | 0.048 | 0.009 | 0.007 | 0.004 | 0.009 | 0.01 |
| | | April | 83574 | -0.221 | 0.009 | 0.018 | -0.006 | -0.028 | -0.002 | 0.004 | 0.009 | 0.01 |
| | 1255 (Q.S. 1 | May | 91104 | -0.221 | -0.002 | 0.016 | 0.007 | -0.033 | -0.002 | 0.004 | 0.009 | -0.01 |
| | Accident Month | July | 91308 | -0.221 | 0.055 | 0.022 | 0.022 | -0.051 | 0.002 | 0.004 | 0.009 | 0.01 |
| | | September | 90267 | -0.221 | -0.076 | 0.007 | 0.009 | 0.043 | -0.002 | 0.004 | 0.000 | -0.019 |
| | | October | 101330 | 0.099 | -0.001 | 0.002 | 0.008 | 0.016 | 0.001 | 0.002 | -0.004 | 0.00 |
| | | November | 102916 | 2.294 | 0.019 | -0.039 | 0.074 | 0.143 | 0.021 | 0.040 | 0.095 | 0.154 |

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4.3.1. Dichotomous quantification

- a) Built-up speed area manifested positive stance/ attribute, but non-built-up speed area contained negative stance.
- b) Carriageway hazards manifested positive stance/ attribute, but non-hazards expressed negative stance.
- c) 'At junction' manifested positive stance, but 'out of junction' had negative stance.
- d) 'Junction control' had positive stance, but 'non-control' had negative stance.
- e) Pedestrian crossing at human control quantificated negative stance, but non-control quantificated positive stance.
- f) Pedestrian crossing at physical facilities quantificated positive stance, but non-physical quantificated negative stance.
- g) Both special conditions and non-conditions quantificated positive stance.

4.3.2. Nominal quantification

- h) Eastern region as well as London, South-West, and South-East of England region, manifests positive stance. On the other hand, North-East region as well as North-West, Yorkshire/ the Humber, East Midlands, and West Midlands, contains negativity.
- i) 'Day light' as well as 'darkness with light unlit', 'darkness without lighting', and 'darkness with lighting unknown' of lighting conditions quantificated positive stance. Only 'darkness with lights lit' quantificated negative stance.
- j) All the categories of 'road type', except 'unknown RT', had negative stance.
- k) 'Raining without high winds' as well as 'snowing without high winds', 'snowing with high winds', 'fog or mist', and 'other/ unknown' of weather conditions had positive quantification. On the other hand, 'fine without high winds', 'fine with high winds', and 'raining with high winds' had negative stance.

4.3.3. Ordinal quantification

- I) All categories of OSGR easting band, except OSE 400-500km, quantificated negative stance.
- m) All categories of OSGR northing band, except OSN 100-200km, quantificated negative stance.
- n) All categories of speed limit zone, except 30 mph, quantificated negative stance.
- **o**) Single casualty per accident had negative stance, but double as well as multiple casualties per accident had positive stance.
- p) Single car per accident had negative stance, but double as well as multiple cars per accident had positive stance.

4.4. Variance Accounted For (VAF) in Variables

The highest VAF in vector coordinates of the first component was in 'built-non-built-up speed area (0.690)' followed by 'speed limi zone (0.652)', 'lighting conditions (0.314)', 'casualty per accident (0.168)', and 'pedestrian crossing at physical-non-physical facilities (0.161)'. England region (0.694) followed by OSGR northing band (0.502), and OSGR easting band (0.397) had the highest in the second component. On the other hand, 'road type (0.678)' had the highest in the third component followed by 'weather conditions (0.586)', 'accident year (0.152)', 'special-non-special conditions (0.007)', 'accident month (0.006)', and 'pedestrian crossing at

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human control-non-control (0.006)'. Further, in the fourth component, 'car per accident (0.526)' had the highest followed by 'junction-non-junction details (0.329)', 'junction controlnon-control (0.169)', 'accident time (0.126)', 'accident day (0.011)', and 'carriageway hazards-non-hazards (0.009)'. These are detailed in Table 4.4 and displayed in Figure 4.4. It displays the coordinates for each item on each dimension in relation to the centroid (0, 0). It is noted that displayed a very small mean coordinate (very close to or below 0.100) indicates these items not contributing substantially to the principal components.

CATPCA Loading plots of eigenvalue (VAF) are as follows:



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Figure 4.4: Loading Plots of Eigenvalue (VAF) in CATPCA Components

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Table 4.4. Variance Accounted For (VAF) in CATPCA of KSI Car Accidents in England Variance Accounted For (VAF) in CATPCA of KSI Car Accidents in England

| | | Centro | id Coor | dinates | | Te | otal (Vec | tor Cod | ordinates | s) |
|---|-------|---------|---------|---------|-------|--------|-----------|---------|-----------|-------|
| | | Dime | nsion | | Maan | | Dimer | nsion | | Total |
| | 1 | 2 | 3 | 4 | mean | 1 | 2 | 3 | 4 | TOLAI |
| Built-non-Built-up Speed Area | 0.690 | 0.070 | 0.002 | 0.037 | 0.200 | 0.690 | 0.070 | 0.001 | 0.037 | 0.798 |
| Speed Limit Zone | 0.739 | 0.071 | 0.005 | 0.046 | 0.215 | 0.652 | 0.055 | 0.003 | 0.043 | 0.753 |
| Lighting Conditions | 0.315 | 0.051 | 0.009 | 0.027 | 0.101 | 0.314 | 0.051 | 0.001 | 0.002 | 0.367 |
| Casualty per KSI Car Accident | 0.168 | 0.019 | 0.001 | 0.135 | 0.081 | 0.168 | 0.019 | 0.001 | 0.135 | 0.323 |
| Pedestrian Crossing at Physical-non-Physical Facilities | 0.162 | 0.003 | 0.013 | 0.015 | 0.048 | 0.161 | 0.003 | 0.007 | 0.014 | 0.185 |
| England Region | 0.273 | 0.712 | 0.030 | 0.005 | 0.255 | 0.200 | 0.694 | 0.008 | < 0.001 | 0.903 |
| OSGR Northing Band | 0.119 | 0.557 | 0.229 | 0.009 | 0.229 | 0.103 | 0.502 | 0.096 | 0.001 | 0.701 |
| OSGR Easting Band | 0.098 | 0.463 | 0.104 | 0.005 | 0.167 | 0.079 | 0.397 | 0.007 | < 0.001 | 0.483 |
| Road Type | 0.059 | 0.043 | 0.678 | 0.039 | 0.205 | 0.035 | 0.033 | 0.678 | 0.029 | 0.775 |
| Weather Conditions | 0.021 | 0.032 | 0.586 | 0.025 | 0.166 | 0.012 | 0.032 | 0.586 | 0.024 | 0.655 |
| Accident Year | 0.003 | 0.003 | 0.220 | 0.025 | 0.063 | 0.002 | 0.001 | 0.152 | 0.021 | 0.175 |
| Special Conditions-non-Conditions at Site | 0.003 | < 0.001 | 0.007 | 0.001 | 0.003 | 0.002 | < 0.001 | 0.007 | 0.001 | 0.010 |
| Accident Month | 0.001 | < 0.001 | 0.007 | 0.001 | 0.002 | <0.001 | < 0.001 | 0.006 | 0.001 | 0.007 |
| Pedestrian Crossing at Human Control-non-Control | 0.002 | < 0.001 | 0.006 | 0.001 | 0.003 | 0.001 | < 0.001 | 0.006 | 0.001 | 0.008 |
| Car per KSI Accident | 0.029 | 0.005 | 0.028 | 0.526 | 0.147 | 0.012 | 0.003 | 0.027 | 0.526 | 0.568 |
| Junction-non-Junction Details | 0.307 | 0.058 | 0.033 | 0.329 | 0.182 | 0.307 | 0.058 | 0.032 | 0.329 | 0.726 |
| Junction Control-non-Control | 0.146 | 0.032 | 0.011 | 0.169 | 0.090 | 0.146 | 0.031 | 0.009 | 0.169 | 0.355 |
| Accident Time | 0.010 | 0.012 | 0.013 | 0.130 | 0.041 | 0.008 | 0.010 | 0.009 | 0.126 | 0.153 |
| Accident Day | 0.009 | 0.003 | 0.003 | 0.014 | 0.007 | 0.008 | 0.003 | 0.002 | 0.011 | 0.024 |
| Carriageway Hazards-non-Hazards | 0.006 | < 0.001 | 0.002 | 0.009 | 0.004 | 0.006 | < 0.001 | 0.002 | 0.009 | 0.017 |
| Active Total | 3.159 | 2.136 | 1.988 | 1.549 | 2.208 | 2.905 | 1.962 | 1.640 | 1.478 | 7.986 |

4.5. Rotated Variance Accounted For (RVAF) in Variables

The rotated VAF had a little change and there was also a little change of variable in component to component. These are detailed in Table 4.5.

| Table 4.5. Rotated | Variance Accounted | For (RVAF) in | n CATPCA of | KSI Car A | Accidents in |
|--------------------|--------------------|---------------|-------------|-----------|--------------|
| England | | | | | |

| Rotated Variance Accounted F | or (RVA | AF) in C | ATPCA | ofKSI | Car Acc | idents i | n Engla | nd | | |
|---|---------|----------|---------|----------|---------|----------|----------|----------|-----------|-------|
| | | Centro | id Coo | rdinates | | T | otal (Ve | ctor Cod | ordinates | s) |
| | | Dime | nsion | | Maan | | Dime | nsion | | Total |
| | 1 | 2 | 3 | 4 | mean | 1 | 2 | 3 | 4 | TOLAI |
| Built-non-Built-up Speed Area | 0.752 | 0.001 | 0.035 | 0.010 | 0.200 | 0.752 | 0.001 | 0.035 | 0.010 | 0.798 |
| Speed Limit Zone | 0.806 | 0.004 | 0.037 | 0.014 | 0.215 | 0.714 | 0.003 | 0.023 | 0.013 | 0.753 |
| Casualty per KSI Car Accident | 0.301 | < 0.001 | 0.022 | < 0.001 | 0.081 | 0.301 | < 0.001 | 0.022 | < 0.001 | 0.323 |
| Lighting Conditions | 0.285 | < 0.001 | 0.111 | 0.006 | 0.101 | 0.278 | < 0.001 | 0.086 | 0.003 | 0.367 |
| Pedestrian Crossing at Physical-non-Physical Facilities | 0.169 | 0.012 | 0.007 | 0.010 | 0.049 | 0.166 | 0.012 | 0.006 | 0.002 | 0.185 |
| England Region | 0.096 | 0.877 | 0.005 | 0.042 | 0.255 | 0.011 | 0.874 | 0.001 | 0.016 | 0.903 |
| OSGR Northing Band | 0.014 | 0.722 | 0.003 | 0.178 | 0.229 | 0.003 | 0.679 | 0.001 | 0.018 | 0.701 |
| OSGR Easting Band | 0.008 | 0.577 | 0.002 | 0.086 | 0.168 | 0.001 | 0.477 | < 0.001 | 0.004 | 0.483 |
| Junction-non-Junction Details | 0.087 | < 0.001 | 0.638 | 0.002 | 0.182 | 0.087 | <0.001 | 0.638 | 0.002 | 0.726 |
| Car per KSI Accident | 0.193 | 0.003 | 0.392 | < 0.001 | 0.147 | 0.180 | 0.003 | 0.386 | < 0.001 | 0.568 |
| Junction Control-non-Control | 0.072 | 0.004 | 0.559 | 0.008 | 0.161 | 0.040 | < 0.001 | 0.312 | 0.003 | 0.355 |
| Accident Time | 0.006 | 0.003 | 0.154 | 0.002 | 0.041 | 0.002 | 0.001 | 0.149 | < 0.001 | 0.153 |
| Accident Day | 0.002 | < 0.001 | 0.026 | < 0.001 | 0.007 | 0.002 | < 0.001 | 0.021 | < 0.001 | 0.024 |
| Carriageway Hazards-non-Hazards | < 0.001 | 0.002 | 0.015 | < 0.001 | 0.004 | < 0.001 | 0.002 | 0.015 | < 0.001 | 0.017 |
| Road Type | 0.025 | 0.005 | 0.021 | 0.782 | 0.208 | 0.001 | 0.003 | 0.002 | 0.769 | 0.775 |
| Weather Conditions | 0.007 | 0.003 | 0.007 | 0.647 | 0.166 | 0.001 | 0.002 | 0.005 | 0.647 | 0.655 |
| Accident Year | 0.003 | 0.005 | 0.004 | 0.239 | 0.063 | 0.001 | 0.002 | 0.001 | 0.171 | 0.175 |
| Special Conditions-non-Conditions at Site | 0.002 | < 0.001 | < 0.001 | 0.010 | 0.003 | < 0.001 | < 0.001 | < 0.001 | 0.009 | 0.010 |
| Pedestrian Crossing at Human Control-non-Control | 0.002 | < 0.001 | < 0.001 | 0.008 | 0.003 | < 0.001 | < 0.001 | < 0.001 | 0.008 | 0.008 |
| Accident Month | 0.001 | < 0.001 | 0.003 | 0.005 | 0.002 | < 0.001 | < 0.001 | 0.002 | 0.005 | 0.007 |
| Active Total | 2.828 | 2.219 | 2.040 | 2.051 | 2.284 | 2.540 | 2.060 | 1.705 | 1.680 | 7.986 |

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4.6. Correlation in Original Variables

Out of 190 unique pairs of twenty original variables (i.e., $20_{c_2} = 190$) in the analysis, only three pairs had greater (> 0.30) or lesser (< -0.30) correlation and such pair of variables are 'junction-non-junction details vs Junction control-non-control ($\rho = -0.966$)', 'speed limit zone vs built-non-built-up speed area ($\rho = 0.464$)', and 'OSGR northing band vs England region ($\rho = 0.399$)'. The correlation matrix of original variables are displayed in Table 4.6.

Table 4.6. Correlation Matrix of Original Variables in CATPCA of KSI Car Accidents in England

| | | Correl | ation M | where we | Orderin al | Variabil | an in CA | TRCA | FK SLC | ar Acele | lants in | England | * | | | | | | | |
|---|--------------|-------------------------------------|--|----------------------------|----------------------------|--|---|--|-------------|-------------------|----------|-------------------|-----------------|-------------------|----------------|-------------------------------|----------------------|--------------|-------------|---------------|
| | coldert Year | Correl eavy peaks on the control | ation M space-prove-provide Memobility | unetan Contral-man-Central | urkton-non-Surkton Details | Adestrary Crossing 9(14,man Contra non-Currier | scheman Crussing at Physical-nun-Physical Facilities 90 | pecial Conditions-non-Conditions at Sale | ngand Ragun | inding Conditions | ents in | Finden Conditions | BGR Easing Band | SDR Northing Band | peed.umit.Zone | sexually per KSI Car Accident | lar per KSI Accident | doldent Time | coldent Day | ccident Month |
| Accident Year | 1.000 | 00 | .0. | | - 2 - | a. | . 0. | | ιu. | | at . | 5 | | 0 | 10 | 0 | .0 | ٩ | ۹. | 4 |
| Built non Built up Speed Area | -0.010 | 1,000 | | | | | | | | | | | | | | | | | | |
| Carriageway Hazards-non-Hazards | -0.020 | -8.044 | 1.000 | | | | | | | | | | | | | | | | | |
| Junction Control-non-Control | -0.031 | -0.285 | 0.053 | 1.000 | | | | | | | | | | | | | | | | |
| Junction-non-Junction Details | -0.005 | 0.298 | -0.050 | -0.966 | 1.000 | | | | | | | | | | | | | | | |
| Pedestrian Crossing at Human Control non-Control | 0.004 | 0.028 | 0.002 | -0.015 | 0.015 | 1.000 | | | | | | | | | | | | | | |
| Pedestrian Crossing at Physical-non-Physical Facilities | 0.074 | 0.234 | -0.022 | -0.176 | 0.181 | 9.060 | 1.000 | | | | | | | | | | | | | |
| Special Conditions-non-Conditions at Site | -0.002 | -0.035 | 0.020 | 0.017 | -8.018 | <0.001 | 0.001 | 1.000 | | | | | | | | | | | | |
| England Region | 0.030 | .0.054 | 0.015 | 0.008 | -0.015 | .0.009 | 0.002 | -0.007 | 1.000 | | | | | | | | | | | |
| Lighting Conditions | 0.038 | -0.138 | -0.010 | 0.050 | 0.022 | 0.017 | 0.067 | 0.012 | 0.031 | 1,000 | 1.121.11 | | | | | | | | | |
| Road Type | -0.051 | 0.130 | -0.002 | 0.027 | -0.025 | 0.008 | 0.076 | -0.031 | -0.012 | 0.027 | 1.000 | | | | | | | | | |
| Weather Conditions | 0.052 | 0.022 | -0.002 | -0.017 | 0.017 | -0.002 | -0.001 | -0.014 | 0.005 | 0.068 | 0.009 | 1.000 | | | | | | | | |
| OCCR Notting Band | 0.025 | -0.041 | 0.005 | 0.034 | -0.022 | -0.001 | -0.017 | 0.003 | -0.052 | 0.004 | 0.014 | 0.021 | 1,000 | 1.000 | | | | | | |
| Social Limit Topo | 0.043 | 0.009 | 0.012 | 0.458 | 0.049 | 8.042 | 0.009 | 0.004 | 0.040 | 0.0624 | 0.134 | 0.011 | 0.052 | 0.073 | 1.000 | | | | | |
| Casualty par KSI Car Accided | 0.042 | 0.290 | 0.003 | 0.005 | 0.100 | 8.015 | .0.105 | 0.024 | 0.040 | 0.003 | 0.028 | 0.020 | 0.015 | 0.048 | .0 101 | 1.050 | | | | |
| Cariner KSLArrident | 0.018 | .0.151 | -0.033 | .0.090 | 0.080 | .8.023 | .0 125 | 0.029 | 0.059 | 6.111 | .0.023 | .0.005 | 0.014 | -0.007 | .0.114 | 0.250 | 1.000 | | | |
| Accident Time | 0.045 | 0.052 | .0.011 | .0.033 | 0.036 | .0.011 | 0.005 | .0.615 | .0.022 | 0.090 | 0.043 | .0.001 | 0.007 | 0.013 | 0.030 | .0 017 | 0.025 | 1.000 | | |
| Acodent Day | -0.017 | 0.021 | .0.003 | .0.004 | 0.000 | 0.001 | 0.010 | .0.005 | .0.001 | 0.021 | 0.007 | 0.005 | 0 001 | -0.002 | 0.014 | -0.019 | .0.010 | 0.034 | 1.005 | |
| Accident Month | 0.017 | 0.005 | 0.002 | 0.004 | 0.004 | 0.002 | -0.001 | <0.001 | 0.002 | 0.057 | 0.001 | 0.027 | 0.003 | -0.004 | -0.007 | 0.005 | 0.013 | 0.009 | 0.002 | 1.000 |
| Dimension | 1 | 2 | 3 | 4 | 5 | 8 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 |
| Eigenvalue | 2.461 | 1.588 | 1.415 | 1.196 | 1.164 | 1,042 | 1.013 | 1.004 | 0.995 | 0.988 | 0.974 | 0.959 | 0.94 | 0.889 | 0.825 | 0.798 | 0.659 | 0.571 | 0.484 | 0.033 |

4.7. Correlation in Transformed Variables

Out of 190 unique pairs of twenty transformed variables (i.e., $20_{c_2} = 190$) in the analysis, only seven pairs had greater (> 0.30) or lesser (< -0.30) correlation and such pair of variables are 'junction-non-junction details vs Junction control-non-control ($\rho = 0.884$)', 'lighting conditions vs built-non-built-up speed area ($\rho = -0.434$)', 'weather conditions vs road type ($\rho = 0.354$)', 'OSGR easting band vs England region ($\rho = -0.535$)', 'OSGR northing band vs England region ($\rho = 0.700$)', 'speed limit zone vs built-non-built-up speed area ($\rho = -0.372$)'. The correlation matrix of transformed variables are displayed in Table 4.7.

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Table 4.7. Correlation Matrix of Transformed Variables in CATPCA of KSI Car Accidents in England

| | C | orrelatio | on Matri | ix of Tra | motorm | ed Varia | ibles in | CATPC | orKS | Car Ac | cidents | in Engl | and | | | | | | | |
|---|-------------------|-------------------------------|---------------------------------|------------------------------|-------------------------------|--|--|---|----------------|-----------------------|-----------|------------------|------------------|--------------------|-----------------|-------------------------------|----------------------|----------------|--------------|-----------------|
| | Accidente Y eater | Built-nen-Built-up Epead Area | Certegeway Hackride-con-Hacards | Arretion Control-non-Control | arretion-non-Junction Details | Pedestran Crassing at Human Contra-non-Carstol | Pedestran Crossing at Physical-nun-Physical Facilities | Special Conditions-con-Conditions of Star | England Regian | Ligrising Constitutes | Goad Type | Neather Dondstme | 05GR Easing Band | 080R Northing Band | Speed Lime Zone | Desually per KBI Car Appldant | Car per KSI Accident | Accident Timit | Accident Day | Accident Months |
| Accident Year | 1 000 | 1.000 | - 7.0 | - | | - | | | | | | | | | | | 1.00 | | | |
| But-ton-Bull-up Speed Area | -0.010 | 1.000 | | | | | | | | | | | | | | | | | | |
| Carriageway Hazards-non-Hazards | -0.021 | -0.026 | 1.000 | 100 | | | | | | | | | | | | | | | | |
| Junction Control-non-Control | -0.072 | 0.272 | -0.048 | 1.000 | 1.1.1.1 | | | | | | | | | | | | | | | |
| Junction-non-Junction Details | -0.005 | 0.296 | -0.055 | 0.884 | 1.000 | | | | | | | | | | | | | | | |
| Pedesthan Creasing at Human Control non-Control | -0.004 | -0.028 | 0.001 | -0.014 | -0.015 | 1.000 | | | | | | | | | | | | | | |
| Pedestrian Crossing at Physical-non-Physical Facilities | 0.074 | 0.234 | -0.025 | 0.101 | 0.101 | -0.060 | 1.000 | | | | | | | | | | | | | |
| Special Conditions non-Conditions at Site | 0.002 | -0.035 | 0.075 | 0.016 | -0.010 | <0.001 | 0.001 | 1000 | | | | | | | | | | | | |
| Englind Region | 0.015 | 0.135 | 0.027 | 0.002 | 0.072 | 0.004 | 0.101 | 0.013 | 0.002 | 1000 | | | | | | | | | | |
| Egning Conditions | 0.000 | -0,636 | 0.029 | -0.194 | 0.212 | 0.010 | -0130 | 0.009 | -0.057 | 1,000 | + | | | | | | | | | |
| North Part Constitute | 0.129 | 0.074 | 0.009 | 0.000 | 0.009 | 0.004 | 0.017 | 0.006 | 0.000 | 0.007 | 0.364 | 1005 | | | | | | | | |
| OSCO Eastern Rand | 0.000 | 0.050 | 0.024 | 0.000 | 0.054 | 0.001 | 0.047 | 0.004 | 0.635 | 0.007 | 0.044 | 0.020 | 1.000 | | | | | | | |
| OSOR Labory Date | 0.025 | 0.075 | 0.025 | 0.013 | 0.041 | 0.001 | 0.085 | 0.005 | 0 700 | 0.000 | 0.045 | 0.036 | 0.237 | 1 000 | | | | | | |
| Speed Light Tops | 0.022 | 0.075 | 0.019 | 0.035 | 0.041 | 0.001 | 0.000 | 0.005 | 0.145 | 4 172 | 0.003 | 0.035 | 0.070 | 0.075 | 1.000 | | | | | |
| Camata per KEI Car Arridant | 0.004 | 0.040 | 0.004 | 0.099 | 0.000 | 0.016 | 0.101 | 0.024 | 0.066 | 0.128 | 0.005 | 0.005 | 0.024 | 0.046 | .0 276 | 1.000 | | | | |
| Carper KSI Acodest | 0.013 | 0.203 | 0.007 | 0.121 | 0.141 | 0.024 | 0.124 | 0.024 | 0.014 | 0.023 | 0.013 | 0.045 | 0.0024 | 0.034 | 0.130 | 0.229 | 1.000 | | | |
| Accident Time | 0.013 | 0.027 | 0.008 | 0.048 | 0.075 | .0.008 | 0.005 | <0.001 | .0.010 | .0.078 | 0.001 | .0.021 | 0.011 | .0.005 | 0.025 | 0.054 | 0.147 | 1 000 | | |
| Accident Day | .0.001 | 0.044 | 0.001 | 0.071 | 0.034 | .0.011 | 0.020 | .0.001 | 0.009 | _Bot7 | 0.001 | -01001 | 0.001 | 0.007 | 0.040 | 0.075 | 0.058 | 0.138 | 1.000 | |
| Accident Month | 0.035 | 0.004 | 0.001 | 0.001 | <0.001 | 0.005 | 0.015 | 0.001 | 0.008 | 0.015 | 0.004 | 0.050 | 0.006 | -0.007 | =0.001 | 0.004 | 0.023 | 0.003 | 0.021 | 1.000 |
| Dimension | 1 | 2 | 3 | 4 | 5 | 8 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 |
| Eigenvalue | 2,951 | 1.941 | 1.605 | 1.438 | 1.167 | 1.074 | 1.064 | 1,004 | 0.985 | 0.968 | 0,916 | 0.851 | 0.837 | 0.769 | 0.679 | 0.644 | 0.632 | 0.204 | 0.171 | 0.112 |
| 1976 1976 1970 | | | Miss | sing white | es were | imputed | with the | mode of | the qual | ntified vi | risble | | | | | | | | | |

4.8. Component Loadings and Rotated Component Loadings

The reporting CATPCA for KSI car accidents is shown in Table 4.8. Also, the CATPCA component loadings plots as well as rotated loadings are displayed in Figure 4.8. The table for Component Loadings shows the coordinates for each item on each dimension and these are plotted in the next element of the output, the scatter plot displayed above-right.

4.8.1. First Categorical Principal Component (CATPC-1)

First categorical principal component was good with internal consistency (³*Cronbach's* $\alpha = 0.7$). Also its eigenvalue was $\lambda_1 = 2.91$. It comprised five out of 20 original variables, but also five out of 20 variables in rotated model (see the report in Table 4.8). The variables in CATPC-1 reformed with increasing for 'built-non-built up speed area' as well as 'speed limit zone', and 'pedestrian crossing at physical-non-physical facilities', having positive associations with first component; but with decreasing for 'lighting conditions' as well as 'casualty per accident', having nagative associations with first component. These variables in CATPC-1 were in the 4-dimensional factor space to best approximate the data in the least square sense.

³ Internal Consistency for Cronbach's Alpha: Excellent ($\alpha \ge 0.9$); Good ($0.7 \le \alpha < 0.9$); Acceptable ($0.6 \le \alpha < 0.7$); Poor ($0.5 \le \alpha < 0.6$); Unacceptable ($\alpha < 0.5$).

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4.8.2. Second Categorical Principal Component (CATPC-2)

Second categorical principal component was poor with internal consistency (*Cronbach's* $\alpha = 0.52$). Also its eigenvalue was $\lambda_2 = 1.962$. It comprised three out of 20 original variables, but as well as same number of original variables in rotated model (see the report). The variables in CATPC-2 reformed with increasing for 'England region' as well as 'OSGR northing band', having positive associations with second component; but with decreasing for 'OSGR easting band' having negative association with second component. These variables in CATPC-2 were in the 4-dimensional factor space for variance-maximising direction orthogonal to CATPC-1.

4.8.3. Third Categorical Principal Component (CATPC-3)

Third categorical principal component was under-poor/ unacceptable with internal consistency (*Cronbach's* $\alpha = 0.41$). Also its eigenvalue was $\lambda_2 = 1.640$. It comprised six out of 20 original variables but as well as same number of original variables in rotated model (see the report). The variables in CATPC-3 reformed with increasing for 'road type' as well as 'weather conditions', and 'accident month', having positive associations with third component; but with decreasing for 'accident year' as well as 'special condition-non-condition at site', and 'pedestrian crossing at human control-non-control', having negative associations with third component. These variables in CATPC-3 were in the 3-dimensional factor space for variance-maximising direction orthogonal to CATPC-1 and CATPC-2.

4.8.4. Fourth Categorical Principal Component (CATPC-4)

Fourth categorical principal component was under-poor/ unacceptable with internal consistency (*Cronbach's* $\alpha = 0.34$). Also its eigenvalue was $\lambda_2 = 1.48$. It comprised six out of 20 original variables but as well as same number of original variables in rotated model (see the report). The variables in CATPC-4 reformed with increasing for 'car per accident' as well as 'junction-non-junction details', 'junction controll-non-controll', 'accident time', 'accident day', having positive associations with fourth component; but with decreasing for 'carriageway hazards-non-hazards', having negative association with fourth component. These variables in CATPC-4 were in the 4-dimensional factor space for variance-maximising direction orthogonal to CATPC-1, CATPC-2, and CATPC-3.

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Table 4.8. Component Loadings in CATPCA of KSI Car Accidents in England Reporting Component Loadings in CATPCA of KSI Car Accidents in England

| Component Loadings | 100 | S | | | Rotated Component Loadings | | | | | | | | |
|---|--------|----------|----------|----------|---|------------|----------|-------------|---------|--|--|--|--|
| 14 A 44 | | Dime | nsion | _ | M. atta | 120 | Dimer | nsion | | | | | |
| Vanable | 1 | 2 | 3 | 4 | Variable | 1 | 2 | 3 | 4 | | | | |
| Built-non-Built-up Speed Area | 0.831 | -0.264 | 0.035 | -0.191 | Built-non-Built-up Speed Area | 0.867 | 0.037 | 0.186 | 0.101 | | | | |
| Speed Limit Zone | 0.808 | 0.236 | 0.053 | -0.207 | Speed Limit Zone | 0.845 | 0.052 | 0.153 | 0.114 | | | | |
| Lighting Conditions | -0.561 | 0.225 | 0.026 | 0.039 | Casualty per KSI Car Accident | -0.549 | 0.008 | 0.147 | 0.006 | | | | |
| Casualty per KSI Car Accident | -0.410 | 0.138 | 0.031 | 0.368 | Lighting Conditions | -0.527 | 0.007 | -0.294 | 0.057 | | | | |
| Pedestrian Crossing at Physical-non-Physical Facilities | 0.401 | -0.052 | .0.083 | -0.119 | Pedestrian Crossing at Physical-non-Physical Facilities | 0,407 | 0.108 | 0.078 | -0.041 | | | | |
| England Region | 0.448 | 0.833 | -0.087 | 0.019 | England Region | 0.104 | 0.935 | 0.037 | 0.127 | | | | |
| OSGR Northing Band | 0.321 | 0.709 | -0.309 | -0.024 | OSGR Northing Band | 0.056 | 0.824 | 0.038 | -0.134 | | | | |
| OSGR Easting Band | -0.281 | -0.630 | 0.085 | 0.002 | OSGR Easting Band | -0.038 | -0.691 | 0.003 | -0.063 | | | | |
| Road Type | 0.186 | 0.181 | 0.823 | 0.172 | Junction-non-Junction Details | 0.294 | 0.009 | 0.799 | 0.042 | | | | |
| Weather Conditions | 0.112 | 0.179 | 0.765 | 0.156 | Car per KSI Accident | -0.424 | 0.050 | 0.621 | 0.014 | | | | |
| Accident Year | -0.042 | -0.027 | -0.389 | -0.144 | Junction Control-non-Control | 0.199 | -0.009 | 0.558 | 0.057 | | | | |
| Special Conditions-non-Conditions at Sile | -0.040 | -0.015 | -0.084 | -0.032 | Accident Time | -0.046 | -0.039 | 0.386 | 0.001 | | | | |
| Accident Month | -0.002 | 0.003 | 0.079 | -0.023 | Accident Day | 0.047 | -0.011 | 0.146 | 0.007 | | | | |
| Pedestrian Crossing at Human Control non-Control | -0.035 | 0.013 | -0.077 | -0.032 | Carriageway Hazards-non-Hazards | 0.018 | -0.048 | -0.122 | 0.005 | | | | |
| Car per KSI Accident | -0.108 | 0.057 | 0.166 | 0.725 | Road Type | 0.023 | 0.058 | -0.043 | 0.877 | | | | |
| Junction-non-Junction Details | 0.554 | -0.241 | -0.180 | 0.574 | Weather Conditions | -0.032 | 0.042 | -0.068 | 0.805 | | | | |
| Junction Control-non-Control | 0.382 | -0.176 | -0.097 | 0.411 | Accident Year | 0.037 | 0.043 | -0.029 | -0.413 | | | | |
| Accident Time | 0.090 | -0.099 | -0.096 | 0.354 | Special Conditions-non-Conditions at Site | -0.015 | -0.010 | -0.017 | -0.097 | | | | |
| Accident Day | 0.089 | -0.055 | -0.044 | 0.104 | Pedestrian Crossing at Human Control-non-Control | -0.011 | -0.008 | -0.017 | -0.088 | | | | |
| Carriageway Hazards-non-Hazards | -0.076 | -0.012 | 0.048 | -0.096 | Accident Month | 0.009 | -0.020 | -0.041 | 0.067 | | | | |
| Variable Principal Normalizat | ton | | | | Rotation Method: Varimax with Kaiser Normalization. Ro | station co | onverged | l in 5 iter | ations. | | | | |
| Model Summary | | | | - 1 | Model Summary | | | | | | | | |
| Cronbach's Alpha | 0.690 | 0.516 | 0.411 | 0.340 | Cronbach's Alpha | 0.647 | 0.541 | 0.477 | 0.358 | | | | |
| Variance Accounted For (Total (Eigenvalue)) | 2.905 | 1.962 | 1.640 | 1.478 | Variance Accounted For (Total (Eigenvalue)) | 2.540 | 2.060 | 1.705 | 1.680 | | | | |
| Total Cronbach's Alpha in 4-dimensions | | 0.9 | 21 | | Total Cronbach's Alpha in 4-dimensions | | 0.9 | 21 | | | | | |
| Total Variance Accounted For (Total (Eigenvalue)) | | 7.9 | 86 | | Total Variance Accounted For (Total (Eigenvalue)) | | 7.9 | 86 | | | | | |
| Case Processing Summary | | | | | | | | | | | | | |
| Valid Active Cases | | | | | 579496 | | | | | | | | |
| Active Cases with Missing Values | | | | | 510064 | | | | | | | | |
| Supplementary Cases | | | | | 0 | | | | | | | | |
| Total | | | | | 1089560 | | | | | | | | |
| Cases Used in Analysis | | | | | 1089560 | | | | | | | | |
| Credit. CA | TPCA V | ersion 2 | 2.0 by L | eiden SP | SS Group, Leiden University, The Netherlands | | | | | | | | |

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Figure 4.8: Scatter Matrix of Components Loadings and Rotated Component Loadings in CATPCA of KSI Car Accidents in England

4.9. Overview in CATPCA for Road KSI Accidents

CATPCA revealed that four-component solution met the interpretability criterion. The 20 variables were reduced to four components that explained 92.1% (total Cronbach's α based on grand total eigenvalue) of the total variance. A Varimax orthogonal rotation was applied to aid interpretability. The rotated solution exhibited 'simple structure' (Thurstone, 1947). The data was consistent with the accident attributes in the 20-variable dataset that was designed to measure with strong loadings of 5-variables on Component-1, 3-variables on Component-2, 6-variables on Component-3, and 6-variables on Component-4. Component loadings of the rotated solution had a little change.

5. Research Findings, Discussions, and Conclusion

The aim of this study was to identify the component structure of road KSI car accidents in England based on categorical variables in STATS19 database for the period of 1979-2015 by applying categorical principal component analysis. Based on 39 potential variables, this study used CATPCA as an alternative to reduce the large number of variables into the four dimensions of KSI car accidents that have been identified. This study proceeded with 33 fit variables after a series of analyses to determine the fit of variables to be selected. Then,

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following the four steps of analysis in the CATPCA, this study reduced and grouped the 20 variables into four principal components. As the data consisted of mainly categorical types (i.e., dichotomous, nominal, and ordinal), the optimal scaling CATPCA allowed this study to jointly analyse and transform these categorical data into numerical values. The aggregated summation of the data of 1089560 cases (where only 579496 cases valid) on these 20 variables was later transformed into component/object scores. These scores are the manifestations of the surrogates of the four components of KSI car accidents identified in this study. These are the best composite scores to use.

- 1) First categorical principal component comprised five out of 20 original variables. It reformed with increasing for 'built-non-built up speed area' as well as 'speed limit zone', and 'pedestrian crossing at physical-non-physical facilities', having positive associations with first component; but with decreasing for 'lighting conditions' as well as 'casualty per accident', having nagative associations with first component.
- 2) Second categorical principal component consisted of three variables that reformed with increasing for 'England region' as well as 'OSGR northing band', having positive associations with second component; but with decreasing for 'OSGR easting band' having negative association with second component.
- 3) Third categorical principal component comprised six variables that reformed with increasing for 'road type' as well as 'weather conditions', and 'accident month', having positive associations with third component; but with decreasing for 'accident year' as well as 'special condition-non-condition at site', and 'pedestrian crossing at human control-non-control', having negative associations with third component.
- 4) Fourth categorical principal component comprised six variables that reformed with increasing for 'car per accident' as well as 'junction-non-junction details', 'junction controll-non-controll', 'accident time', 'accident day', having positive associations with fourth component; but with decreasing for 'carriageway hazards-non-hazards', having negative association with fourth component.

This research leads a road car safety practice/ policy as a key policy priority that should therefore be to plan for the long-term prevention of road car accidents. The identified significant variables leading KSI car accidents, can be taken special attention so that KSI car accidents can be reduced. This research can be used to develop targeted interventions aimed at road safety practice/ policy. The findings of this study have several important implications for future practice. These findings are dynamic if policymakers are to be able to identify those individuals at greatest threat of KSI car accident involvement. Policies to reduce the KSI car accidents and associated casualties will remain unnecessarily high for certain individuals in the society, and as a society people will all suffer. Where there is an alert today, there is an alive tomorrow. Stay Alive – Think and Drive.

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